



# THE MOTION OF A POINT MASS ALONG A STRING†

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(Received 23 March 2000)

As a supplement to results obtained earlier [1], the general integral of motion of a point mass along a string is determined, and the influence of friction is evaluated. © 2001 Elsevier Science Ltd. All rights reserved.

The problem of the motion of a point mass along a string was considered in [1] as an example of a mechanical system for which Zhukovskii's method [2] can be used to determine the particular integral of motion.

## 1. THE GENERAL INTEGRAL OF MOTION

We will consider, as previously [1], the plane motion of a point mass (a bead) along an elastic weightless thread (a string) stretched between two fixed points. In the plane of motion we will fix a stationary system of coordinates  $Oxy$  so that the points where the string is fastened lie symmetrically on the  $x$  axis at a distance  $l$  from the origin of coordinates.

Let  $r_1$  and  $r_2$  be the distances from the bead to the right-hand and left-hand fastening points, respectively, let  $g$  be the coefficient of tensile stiffness of the string, and let  $\Delta$  be the preliminary tension of the string. Then, the potential energy of the string,  $V$ , is given by the formula

$$V = \frac{1}{2} g[(r_1 + r_2 + \Delta - 2l)^2 - \Delta^2] \tag{1.1}$$

Here the misprint in [1] has been corrected.)

This problem is similar to the well-known problem of two fixed centres [3]. However, to separate the variables, the introduction of new time is also required.

After the introduction of the dimensionless coordinates

$$q_1 = \frac{r_1 + r_2}{2l}, \quad q_2 = \frac{r_1 - r_2}{2l} \quad (-1 \leq q_2 \leq 1 \leq q_1 \leq \infty)$$

the potential energy, the kinetic energy, and the Hamilton–Jacobi equation will respectively take the form

$$\begin{aligned} V &= \frac{1}{2} g[(2lq_1 + \Delta - 2l)^2 - \Delta^2] \\ T &= \frac{1}{2} l^2 m(q_1^2 - q_2^2) \left( \frac{\dot{q}_1^2}{q_1^2 - 1} + \frac{\dot{q}_2^2}{1 - q_2^2} \right) \\ (q_1^2 - 1) \left( \frac{\partial W}{\partial q_1} \right)^2 + (1 - q_2^2) \left( \frac{\partial W}{\partial q_2} \right)^2 &= 2l^2 m(h - V)(q_1^2 - q_2^2) \end{aligned}$$

where  $h$  is the energy constant.

To separate the variables, we will introduce a new time according to the formula

$$dt = \sqrt{q_1^2 - q_2^2} d\tau \tag{1.2}$$

This replacement is one-to-one only when  $q_1 = 1$  and  $|q_2| = 1$  (at the points where the string is fastened).

The Hamilton–Jacobi equation becomes

$$\begin{aligned} (q_1^2 - 1) \left( \frac{\partial W}{\partial q_1} \right)^2 + (1 - q_2^2) \left( \frac{\partial W}{\partial q_2} \right)^2 &= -l_1 q_1^2 + l_2 q_1 + l_3 \\ l_1 &= 4gml^4, \quad l_2 = 4mg l^3(2l - \Delta), \quad l_3 = 2ml^2(h - 2gl(l - \Delta)) \end{aligned}$$

†*Prikl. Mat. Mekh.* Vol. 65, No. 1, pp. 169–172, 2001.

Assuming  $W = W_1(q_1) + W_2(q_2)$ , we obtain the system of equations

$$(q_1^2 - 1) \left( \frac{\partial W_1}{\partial q_1} \right)^2 = -l_1 q_1^2 + l_2 q_1 + l_3 - c_1, \quad (1 - q_2^2) \left( \frac{\partial W_2}{\partial q_2} \right)^2 = c_1$$

where  $c_1$  is an arbitrary constant ( $c_1 > 0$ ). We will write its solution

$$W = \int \sqrt{\frac{l_3 + l_2 q_1 - l_1 q_1^2}{q_1^2 - 1}} dq_1 + \sqrt{c_1} \arcsin q_2$$

and the solution for the generalized coordinates and momenta

$$\frac{\partial W}{\partial c_1} = C_1, \quad \frac{\partial W}{\partial h} = \tau - C_2, \quad \frac{\partial W}{\partial q_1} = p_1, \quad \frac{\partial W}{\partial q_2} = p_2$$

where  $C_1$  and  $C_2$  are arbitrary constants, or in expanded form

$$q_2 = \sin \left[ \sqrt{c_1} \left( \frac{\tau + C_2}{l^2 m} - C_1 \right) \right] \quad (1.3)$$

$$\frac{dq_2}{d\tau} = \frac{\sqrt{c_1} \sqrt{1 - q_2^2}}{l^2 m}, \quad t = \int_0^\tau \sqrt{q_1^2(\tau) - q_2^2(\tau)} d\tau$$

$$I \equiv \int [(q_1^2 - 1)(l_3 + l_2 q_1 - l_1 q_1^2)]^{-1/2} dq_1 = \frac{\tau + C_2}{l^2 m}$$

$$\frac{dq_1}{d\tau} = \sqrt{\frac{(q_1^2 - 1)(l_3 + l_2 q_1 - l_1 q_1^2)}{l^2 m}}$$

When investigating the motions of a point close to the  $x$  axis, the quantity  $u^2 = q_1 - 1$  is close to zero (the product  $g\Delta$  is large). Therefore, with some error, it is possible to simplify the elliptic integral

$$I = 2 \int \left[ (2 + u^2) \left( l_4 - \frac{l_1}{l} \Delta u^2 - l_1 u^4 \right) \right]^{-1/2} du =$$

$$= \int (2l_4 - l_5^2 u^2)^{-1/2} du = \frac{1}{l_5} \arcsin \frac{l_5 u}{\sqrt{2l_4}}$$

$$l_4 = 2l^2 mh - c_1, \quad l_5^2 = 8l^3 mg\Delta - 2l^2 mh + c_1$$

and to write an approximate solution for  $q_1$  in explicit form

$$q_1 = \frac{2l_4}{l_5^2} \sin^2 \frac{l_5(\tau + C_2)}{2l^2 m} + 1$$

## 2. THE STRENGTH OF THE STRING

An important characteristic of the system, from the viewpoint of strength, is the maximum tension of the string  $r_1 + r_2 - 2l$ , an estimate of which can be obtained from an estimate of the range of possible motion

$$g[(r_1 + r_2 - 2l + \Delta)^2 - \Delta^2] < 2h$$

For maximum tension, it is also possible to provide an estimate in the case of a sudden deceleration of a point on the string

$$V_0 = \frac{2El^2(x - a_0)^2 + y^2}{(l_2 - a_0^2)(2l - \Delta)} + E[2l - (r_1 + r_2)] < h$$

where  $E$  is the modulus of elasticity of the string, related to its unit cross-section area and  $a_0$  is the abscissa of a heavy point fixed on the string in the rest position. An expression for the potential energy  $V_0$  can be obtained, for example, by moving a heavy point fixed on the string from the rest point to the point  $(x, 0)$  along the  $x$  axis, and then moving it parallel to the  $y$  axis to the point  $(x, y)$  at which the deceleration occurred.

### 3. THE INFLUENCE OF DRY FRICTION ON THE MOTION OF A POINT

For applications, it may also be of interest to take into account dry friction during the motion of a point along the string.

The tension forces of the string

$$Q = \frac{\partial V}{\partial q_1} = g(2lq_1 - 2l + \Delta)$$

acting on a heavy point along the directions  $r_1$  and  $r_2$  create an equivalent force directed along the bisector of the angle  $\alpha$  between the directions  $r_1$  and  $r_2$ :

$$F = 2Q \cos \frac{\alpha}{2} = 4gl(2lq_1 - 2l + \Delta) \sqrt{\frac{q_1^2 - 1}{q_1^2 - q_2^2}}$$

which generates a friction force  $\mu F$ , where  $\mu$  is the coefficient of dry friction. The latter largely prevents any change in the coordinate  $q_2$  (during motions close to the  $x$  axis, i.e. when  $q\Delta$  is large).

We will write the Lagrange equation for this system

$$\begin{aligned} \frac{q_1^2 - q_2^2}{q_1^2 - 1} \ddot{q}_1 + \frac{q_2^2 - 1}{(q_1^2 - 1)^2} q_1 \dot{q}_1^2 - \frac{2q_2}{q_1^2 - 1} \dot{q}_1 \dot{q}_2 + aq_1 - b &= 0 \\ \frac{q_1^2 - q_2^2}{1 - q_1^2} \ddot{q}_2 + \frac{q_1^2 - 1}{(1 - q_2^2)^2} q_2 \dot{q}_2^2 - \frac{2q_1}{1 - q_2^2} \dot{q}_1 \dot{q}_2 &= -2\mu(aq_1 - b) \sqrt{\frac{q_1^2 - 1}{q_1^2 - q_2^2}} \text{sign } \dot{q}_2 \\ a = \frac{4g}{m}, \quad b = \frac{2g(2l - \Delta)}{lm} \quad (a > b > 0) \end{aligned} \tag{3.1}$$

Regarding  $\mu$  as a small parameter on sections where  $\dot{q}_2$  is of constant sign, and taking into account the presence of a complete integral of the generating system, according to perturbation theory it is possible to find a solution for the perturbed system by differentiation operations and by taking quadratures. Here, very lengthy expressions arise, and it is more convenient to use the method of successive approximations.

Making a replacement of variables, which is used on changing to Hamilton's equations, we transform system (3.1) to the form

$$\begin{aligned} \dot{q}_1 = \frac{(q_1^2 - 1)p_1}{q_1^2 - q_2^2}, \quad \dot{q}_2 = \frac{(1 - q_2^2)p_2}{q_1^2 - q_2^2}, \quad p_1 = -\frac{(1 - q_2^2)q_1 p_2^2}{(q_1^2 - q_2^2)^2} - aq_1 + b \\ \dot{p}_2 = \frac{(q_1^2 - 1)q_2 p_2^2}{q_1^2 - q_2^2} - 2\mu(aq_1 - b) \sqrt{\frac{q_1^2 - 1}{q_1^2 - q_2^2}} \text{sign } \dot{q}_2 \end{aligned} \tag{3.2}$$

where  $p_1$  and  $p_2$  are generalized momenta.

Suppose that, close to the right-hand support, a velocity impulse  $v$  was imparted to the heavy point in a direction similar to the direction on the left-hand support, i.e.

$$q_1 = 1 + \varepsilon_1, \quad q_2 = -1 + \varepsilon_2, \quad \dot{q}_1 = \varepsilon_3, \quad \dot{q}_2 = v \quad \text{when } t = 0$$

where  $\varepsilon_1, \varepsilon_2$  and  $\varepsilon_3$  are small quantities and  $\varepsilon_1 > 0$  and  $\varepsilon_2 > 0$ . It will also be necessary to determine the time  $t^*$  before the point stops ( $\dot{q}_2(t^*) = 0$ ) and the coordinate  $q_2(t^*)$  if it turns out that  $t^* < t_1$ , where  $t_1$  is the time of motion of the point up to the specified neighbourhood of the left-hand support when there is no friction. In this case, the factor  $\text{sign } \dot{q}_2$  in system (3.2) will be replaced by unity.

Taking as the zero approximation the generating solution  $q_{10}, q_{20}, p_{10}$  and  $p_{20}$ , for a first approximation we obtain

$$q_{11} = q_{10}, \quad q_{21} = q_{20}, \quad p_{11} = p_{10}, \quad p_{21} = p_{20} - p_3$$

$$p_3 = 2\mu \int_0^t (aq_{10} - b) \sqrt{\frac{q_{10}^2 - 1}{q_{10}^2 - q_{20}^2}} dt$$

Using the fact that the explicit form of  $q_{10}$  and  $q_{20}$  as a function of  $\tau$  is known, and taking into account relation (1.2), we obtain

$$p_3 = 2\mu \int_0^t (aq_{10} - b) \sqrt{q_{10}^2 - 1} dt \quad (3.3)$$

In the second approximation

$$q_{22} = \int_0^t \frac{1 - q_{20}^2}{q_{10}^2 - q_{20}^2} p_{21} dt$$

From relations (3.2) it can be seen that  $\dot{q}_{22} < p_{20} - p_3$ . If the equation  $p_3 = p_{20}$  in relation to  $t$  has a positive solution, smaller than  $t_1$ , it will approximately represent the quantity  $t^*$ .

The expression for  $p_3$  after integration is fairly lengthy. Therefore, for  $p_3$  we will make an upper estimate. Since  $q_1 \leq q_{1a}$ , where  $q_{1a} = 2l_4/l_5^2 + 1$  is the amplitude value of the solution  $q_{10}$ , it follows that

$$p_3 < 2\mu(aq_{1a} - b) \sqrt{q_{1a}^2 - 1} t \quad \text{и} \quad t^* \cong \nu \left[ 2\mu(aq_{1a} - b) \sqrt{q_{1a}^2 - 1} \right]^{-1}.$$

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Translated by P.S.C.